Assessing the soil type and layering in settlement of the soil under foundations by using Artifical Neural Network

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Abstract: There are defined Theoretical and empirical relationships for predicting settlement of shallow foundation on soils which in spite of the computational complexity, do not predict with high accuracy. Nowadays, artificial neural networks can be used for predicting the settlement of shallow foundation with lower computational complexity and higher accuracy. Modeling 27 samples of Shallow foundations on sandy soil under 14 types of Uniformly distributed load with different length to width ratio, using Plaxis program, the following settlement were calculated. The geotechnical information is obtained from the speculation surrounding the city of Babol. A neural network is designed using the data obtained from the Plaxis program to estimate the settlement of shallow foundation. Plaxis program analyzed the network by model samples. As you know, the neurons in the hidden layer of a neural network is an optimal value so With different values can be used to model the network was designed to optimize the optimal number of neurons in the hidden layer is 350. By changing the value of the friction angle of a soil sample in neural network models, we found that Increase the friction angle of a soil sample to a soil layer will reduce the Settlement and This is due to the increased contact area between the particles and better distribution of stress in a layer of soil to other layers happen.

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1. Introduction

Proper foundation design depends on accurate prediction of the meeting and its distribution. Factors such as material type and hardness of the Earth, Width, and depth,... Have an effect on the amount and distribution of foundation settlement.

Today, several classical equations for calculation of foundation settlement of shallow foundation engineering books available. These relationships are often based on experience or based on elasticity theory are presented. Considering various factors which influence this case, unfortunately, the use of this relationship, with no satisfactory results. In recent years the trend toward computerized tools that are similar to biological nervous systems of the body are increased. These tools are known as artificial neural networks anb Almost all branches of science and engineering applications have been increasing. As a result, the neural network in less time and with good accuracy can be used to solve engineering problems.

1-1- Geography of Babol

The city is located approximately 20 kilometers south of Caspian Sea on the west bank of Babol Rud River and receives abundant annual rainfall. Babol borders Babolsar to the north, Qaem Shahr and Savad Kooh to the east, and Amol to the west. Babol University is famous for its spectacular scenery.



Figure 1. Geography of Babol

2. Materials and methods

2-1- Introducing the soil parameters required for the plaxis program

Due to changes in soil parameters named in the report and geotechnical soil sampling variability expressed, total of 10 soil types have been analyzed, so All samples of the geotechnical characteristics and application requirements Plaxis Program, Displayed in tables 1(a...d) and Concrete parameters for shallow foundations are shown in Tables 1-e.

The data used in presented research, includes borehole logs (data collected from digging boreholes) bored in the study area Figure1and is collected by different institutions for different research purposes (Kusano et al., 1988). The database includes more than 40 borehole logs in an area of more than 6 km2 from Babol zone.

From the total of 40 raw borehole data, only 30 logs with a depth range of 10–30 m were acceptable for using in ANN model. The regular tests were

performed on the samples. The available data set is divided into three sets, namely training, validation, and test sets, based on random selection.

By this division the validity of the model could be examined in a more comprehensive manner. To identify the layers of the soil, geotechnical information obtained from boreholes drilled were used in Town of Babylon These data are shown in figures 2-a and 2-b.

Geotechnical parameters obtained from boreholes drilled in the city of Babylon that have been used are shown in Table 1.

| Field Description of Soils | Depth (m) | Sample | SPT blows count (N) | % Passing Sieve No. 200 | € Moisture % Content | T Liquid Limit | Hastic Limit | Soil Classification | Unconfined E Compression (kg/cm ²) | Internal Friction angle | o Cohesion (kg/cm ²) |
|-----------------------------------|------------|--------------|--------------------------------|----------------------------|----------------------|-------------------|-----------------|------------------------|--|--|-------------------------------------|
| Fa | -0 -1 | | | | | | | | | | |
| | -1 - | SPTI | 2/15, 2/15, 3/18 5/33.cm) | | 27.0 | 32.8 | 21.9 | CL | | - | |
| Meduim stiff lean clay | 2 - | - V1 - D1 | | 92.4 95.3 92.4 | | | | CL . CL CL | | | 0.96 |
| Silly fine sand | -3 - | SPT2 | 3/15, 3/15, 4/18 (7/33 cm) | | 26.2 23.7 | 42.1 | 21.2 | CL ML | 0.78 | | |
| Meduim stiff lean clay | 4 | - V2 | | 95.0 97.5 | 37.8 | | | CL CH | | | 0.74 |
| Stiff fat clay | 5 | ELLAS V3 | 3/18, 4/15, 5/15 (9/30 cm) | | - | | 23.3 | сн сн | 1.70 | | 1.38 |
| | 6 - | - 03 | | 95.7 | 28.1 | | | сн | | | |
| Mudium stiff lean clay | | SPT4 | 2/15, 4/15, 7/15 (11/30 cm) | 95.4 | 27,3 | 2 46. | 8 21.2 | CL | 1.0 | | |
| | . 8 - | 1 1 1 | | 90 | 35. | 1 | | CL | | | 0.53 |
| Sandy silt and silty fine sand | 9 . 9 . | SPT6 | 3/20, 4/15, 5/15 (9/30 cm) | 5 54.3 | 7 23. | 9 28 | .1 NP | ML | | | |
| | E_10 | | | | | | | | | | |

Figure 2-a. borehole log (A) from test borehole

| Field Description of Soils | Depth (m) | Sample | SPT blows count (N) | % Passing Sieve No. 200 | Moishire Content | T Liquid Limit | 1d Plastic Limit | Sol Classification | Unconfined E Compression (kg/em ²) | Internal Friction angle | o Cahesion (kalani) |
|-----------------------------------|-----------|--------|--------------------------------|----------------------------|---|-------------------|---------------------|-----------------------|--|--|------------------------|
| Sandy silt and silty fine sand | 10 | | | | | | | | | | |
| Silty fine sand along | -11 - | SPT6 | 4/15, 4/15, 4/15 (8/30 cm) | 42.9 | 21.4 | 26 | 15.3 | SC | | | |
| with layers of sity day | - 12- | - D4 | | 39 | 26.1 | | | SM | | | |
| | 13 | 211qS | 3/15, 8/15, 8/15 (16/30 cm) | 1.0.10 | 22.8 | 26.1 | NP | SM CH | | | |
| Stiff fat.clay | | | | | | | | | | | |
| | 14 | SPT8 | 5/16, 9/15, 11/1 (20/30 cm) | 5 98.4 | 28.4 | | | СН | 1.56 | | |
| | 15_ | 05 | | 95.3 | 2 28.1 | | | сн | | | |
| Sbff dark fat clay | 16- | SPT8 | 3/15, 6/16, 8/1; (14/29 cm) | 99. | 4 29.5 | 59.2 | 24.3 | сн | 2.4 | | |
| | 17. | De | 1 | 91. | 4 31.6 | 5 | | СН | | | |
| Medium stiff day | 18- | SPT10 | 2/16, 4/15, 5/1 (9/32 cm) | 84. | 8 29. 1 26 | 30. | 9 21.3 | CL 2 CL | | | |
| End of baring | 19 | - | | | | | | | | | |
| | 20 | | | | | | | | | | |

Figure 2- b. borehole log (B) from test borehole

| | | | | | SC | | | | | |
|----------------------------|--------------------------------|---------------------------|------|---|---------------------|---------------------------|------|---------------------|--------------------|-------------------------------|
| $\gamma_d(\frac{KN}{m^3})$ | $\gamma_{sat}(\frac{KN}{m^3})$ | $E_{ref}(\frac{KN}{m^2})$ | v | ψ | $G(\frac{KN}{m^2})$ | $E_{oed}(\frac{KN}{m^2})$ | φ | $C(\frac{KN}{m^2})$ | $V_s(\frac{M}{s})$ | $V_p\left(\frac{M}{s}\right)$ |
| 16 | 19 | 20000 | 0.25 | 1 | 8000 | 24000 | 31.2 | <mark>0.44</mark> | 70 | 121.2 |

| | | | | | SC2 | | | | | |
|----------------------------|--|---------------------------|-----|---|---------------------|---------------------------|----|---------------------|--------------------|--------------------|
| $\gamma_d(\frac{KN}{m^3})$ | Y sat(^{KN} /m ³) | $E_{ref}(\frac{KN}{m^2})$ | ν | ψ | $G(\frac{KN}{m^2})$ | $E_{oed}(\frac{KN}{m^2})$ | φ | $C(\frac{KN}{m^2})$ | $V_s(\frac{M}{s})$ | $V_p(\frac{M}{s})$ |
| 16 | 19 | 30000 | 0.3 | 1 | 11540 | 40380 | 36 | 0.44 | 84.07 | 157.3 |

| | | | | | SC3 | | | | | |
|----------------------------|---------------------------------------|---------------------------|-----|---|---------------------|---------------------------|------|---------------------|--------------------|--------------------|
| $\gamma_d(\frac{KN}{m^3})$ | Ysat(^{KN} /m ³) | $E_{ref}(\frac{KN}{m^2})$ | ν | ψ | $G(\frac{KN}{m^2})$ | $E_{oed}(\frac{KN}{m^2})$ | φ | $C(\frac{KN}{m^2})$ | $V_s(\frac{M}{s})$ | $V_p(\frac{M}{s})$ |
| 16 | 19 | 15000 | 0.3 | 1 | 5769.231 | 20190 | 37.5 | 0.44 | 59.44 | 111.2 |

| | | | | | SC4 | | | | | |
|-----------------------|---|---------------------------|-----|---|---------------------|---------------------------|----|---------------------|--------------------|--------------------|
| $Y_d(\frac{KN}{m^3})$ | Ysat(^{KN} m ³) | $E_{ref}(\frac{KN}{m^2})$ | v | ψ | $G(\frac{KN}{m^2})$ | $E_{oed}(\frac{KN}{m^2})$ | φ | $C(\frac{KN}{m^2})$ | $V_s(\frac{M}{s})$ | $V_p(\frac{M}{s})$ |
| 16 | 19 | 20000 | 0.3 | 1 | 7692.308 | 26920 | 39 | 0.44 | 68.640 | 128.4 |

| | | | | | SM | | | | - | - |
|----------------------------|--------------------------------|---------------------------|-----|-----|---------------------|---------------------------|------|---------------------|--------------------|--------------------|
| $\gamma_d(\frac{KN}{m^3})$ | $\gamma_{sat}(\frac{KN}{m^3})$ | $E_{ref}(\frac{KN}{m^2})$ | ν | ψ | $G(\frac{KN}{m^2})$ | $E_{oed}(\frac{KN}{m^2})$ | φ | $C(\frac{KN}{m^2})$ | $V_s(\frac{M}{s})$ | $V_p(\frac{M}{s})$ |
| 18 | 20 | 13000 | 0.3 | 3.7 | 5000 | 17500 | 33.7 | 1 | 52.17 | 97.610 |

| | | | | | SM2 | | | | | |
|----------------------------|--------------------------------|---------------------------|-----|-----|---------------------|---------------------------|------|---------------------|--------------------|--------------------|
| $\gamma_d(\frac{KN}{m^3})$ | $\gamma_{sat}(\frac{KN}{m^3})$ | $E_{ref}(\frac{KN}{m^2})$ | ν | ψ | $G(\frac{KN}{m^2})$ | $E_{oed}(\frac{KN}{m^2})$ | φ | $C(\frac{KN}{m^2})$ | $V_s(\frac{M}{s})$ | $V_p(\frac{M}{s})$ |
| 18 | 20 | 14000 | 0.3 | 3.7 | 5384.615 | 1885 <mark>0</mark> | 33.7 | 0 | <mark>54.14</mark> | 101.3 |

| | | | | | SM3 | | | | | |
|----------------------------|--------------------------------|---------------------------|------|-----|---------------------|---------------------------|----|---------------------|--------------------|--------------------|
| $\gamma_d(\frac{KN}{m^3})$ | $\gamma_{sat}(\frac{KN}{m^3})$ | $E_{ref}(\frac{KN}{m^2})$ | v | ψ | $G(\frac{KN}{m^2})$ | $E_{oed}(\frac{KN}{m^2})$ | φ | $C(\frac{KN}{m^2})$ | $V_s(\frac{M}{s})$ | $V_p(\frac{M}{s})$ |
| 18 | 20 | 21000 | 0.28 | 3.7 | 8203.125 | 26850 | 40 | 1 | 66.83 | 120.9 |

Table 1-b : Silty sandy soil geotechnical parameters (SM)

| | SP1 | | | | | | | | | | | | |
|----------------------------|--------------------------------|---------------------------|-----|---|---------------------|---------------------------|----|---------------------|--------------------|--------------------|--|--|--|
| $\gamma_d(\frac{KN}{m^3})$ | $\gamma_{sat}(\frac{KN}{m^3})$ | $E_{ref}(\frac{KN}{m^2})$ | v | ψ | $G(\frac{KN}{m^2})$ | $E_{oed}(\frac{KN}{m^2})$ | φ | $C(\frac{KN}{m^2})$ | $V_s(\frac{M}{s})$ | $V_p(\frac{M}{s})$ | | | |
| 16 | 20 | 3000 0 | 0.3 | 3 | 11540 | 40380 | 37 | 0.2 | <mark>84.07</mark> | 157.3 | | | |

Table 1 - c : Poor sandy soil geotechnical parameters aggregation (SP)

| | | | | | Sp2 | | | | | |
|----------------------------|--------------------------------|---------------------------|-----|---|---------------------|---------------------------|----|---------------------|--------------------|--------------------|
| $\gamma_d(\frac{KN}{m^3})$ | $\gamma_{sat}(\frac{KN}{m^3})$ | $E_{ref}(\frac{KN}{m^2})$ | V | ¥ | $G(\frac{KN}{m^2})$ | $E_{oed}(\frac{KN}{m^2})$ | φ | $C(\frac{KN}{m^2})$ | $V_s(\frac{M}{s})$ | $V_p(\frac{M}{s})$ |
| 18 | 20 | 100000 | 0.3 | 3 | <u>38460</u> | 134600 | 37 | 1 | 144.7 | 270.7 |

Table 1 - c : Poor sandy soil geotechnical parameters aggregation (SP)

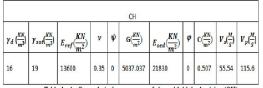


Table 1- d : Geotechnical parameters of clay with high plasticity (CH)

| | | | Concrete | | | |
|---------------------------|---------------------------|---------------|---------------------|---------------------------|--------------------|--------------------|
| Yunsat($rac{KN}{m^3}$) | $E_{ref}(\frac{KN}{m^2})$ | ν | $G(\frac{KN}{m^2})$ | $E_{oed}(\frac{KN}{m^2})$ | $V_s(\frac{M}{s})$ | $V_p(\frac{M}{s})$ |
| 24 | 5000 | 0.25 | 2000 | 6000 | 28 | 49 |
| | Т | ahle 1-e : Ge | otechnical na | rameters of co | mcrete | |

2-2- Modelin in Plaxis Program

The mesh and boundary conditions (soil behavior using finite element method), for the simulation executable work, three-phase program is defined as follows:

1- Definition of soil for Plaxis.

2- Declared shallow foundation material and foundation for program.

3- Load on the foundation.

| General Parameters Mutpliers Preview Phase Total multipliers at the end of previous loading step Start from phase: 2 - «Phase 3> Start from phase: 2 - «Phase 2> Image: 1000 PMax 0.000 Start from phase: 2 - «Phase 2> Image: 1000 Force-X: 0.000 Start from phase: 2 - «Phase 2> Image: 1000 Force-X: 0.000 Start from phase: 2 - «Phase 2> Image: 1000 Force-X: 0.000 Start from phase: 2 - «Phase 2> Image: 1000 Force-X: 0.000 Start from phase: 2 - «Phase 10.000 Force-X: 0.000 Stiffness: 0.000 Start from process of current step 0.001 Current step: 30 Max. sterations: 60 Current step: 30 Max. sterations: 60 Boerance: 0.010 Calc. time: Plastic N/A Plastic 10 Inaccurate 13 Tolerated: Intable phase 0 0 N/A 10 Plastic 3 Cap/Hard points: 0 Apex points: | Input Output Curves | 🕒 🔒 | <u>ه</u> | • | Plaxis 8.1 Plastic Calculation - | SC - Plane | Strain | | | |
|--|---|--------------------|------------|-------------|----------------------------------|-----------------------|-----------------|------|----------------------------|--------------------|
| Start from phase: 2 - «Phase 2> Image: 1 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - | Phase | | | | | | - | | alculation progre Stage | 295 |
| $\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$ | | | | - | Σ -MloadB: 1.000 | Force-X: | 0.000 | | | |
| Identification Phase no. Start from Calculation Initial phase 0 0 N/A N/A Iteration trace 10 Tolerance: 10 | - | limate state fully | reached | | Σ-Msf: 1.000 | Time: | 0.000 | ł | 1 months | |
| Identification Phase no. Start from Calculation Initial phase 0 0 N/A | | | | * | Current step: 39 Iteration: 6 | Max. ste Max. iter | ations: 60 | Deco | ent | 143 100 ' 43 |
| Initial phase 0 0 N/A Plastic interface points: 0 Inaccurate 0 Tolerated: | | | | | | | | | | |
| Initial phase 0 0 N/A | Identification | Phase no. | Start from | Calculation | | | | | | 3 |
| → <phase 1=""> 1 0 Plastic Tension points: 3 Cap/Hard points: 0 Apex points:</phase> | Initial phase | 0 | 0 | N/A | | | | | | |
| | <phase 1=""></phase> | | | Plastic | Tension points: | 3 C | ap/Hard points: | 0 | Apex points: | |
| | → <phase 2=""></phase> | | | Plastic | | | | | | Cancel |
| 👷 <phase 3=""> 3 2 Plastic</phase> | All | 3 | 2 | Plastic | | | | _ | | ancer |

| 🚆 Plaxis 8.2 Calculati | ons - SC.plx | | | | | | x |
|--|---|------------|-------------|---|--------|--------|---|
| File Edit View C | alculate Help | • | | | | | |
| Input Output Curves | 🗠 🔒 | | 🕂 Outpu | t | | | |
| General Parameters Phase Number / ID.: Start from phase Log info Prescribed ulti | 3 <pha< th=""><th>ase 3></th><th>x</th><th>Calculation type Plastic Advanced Comments Parameters Parameters</th><th>1</th><th></th><th></th></pha<> | ase 3> | x | Calculation type Plastic Advanced Comments Parameters Parameters | 1 | | |
| | | | | 📮 Next 🗮 | Insert | Delete | |
| Identification | Phase no. | Start from | Calculation | Loading input | Time | Water | F |
| Initial phase | 0 | 0 | N/A | N/A | 0.00 | 0 | C |
| ✓ <phase 1=""></phase> | 1 | 0 | Plastic | Staged construction | 0.00 | 0 | 1 |
| ✓ <phase 2=""></phase> | 2 | 1 | Plastic | Staged construction | 0.00 | 0 | 4 |
| 💉 <phase 3=""></phase> | 3 | 2 | Plastic | Staged construction | 0.00 | 0 | € |
| • | | | | | | | ł |

Figure 3.Calculations window

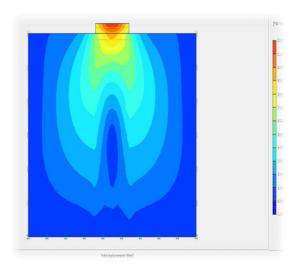


Figure 4-a. General Settelement of the Foundation

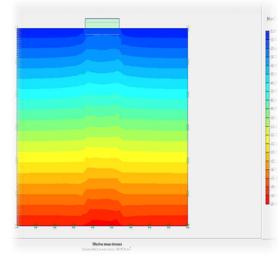


Figure 4-b. Effective stress in the soil

2-3- Define the network Initial input

In ANN forecasting models, 60% of the records are selected as training, 30% are taken for test for final evaluation, and the remaining 10% are used for

validation or monitoring the performance of the model during the training phase.

For Neural Network Training, We consider three inputs:

1-Distributed load: $q (KN/m^2)$

- 2-Standard Penetration Number (SPT)
- 3- Ratio of length to width of the foundation: L/B

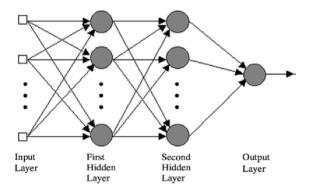


Figure 5: A three-layer feed-forward neural network structure.

2-3-1 Calculate of the Standard Penetration Number modified

This table 2, that Introduced in 1956 by Meyerhof is used for many of the papers Indicates that Empirical relationship between the angle of internal friction of soil and SPT.

Table2: The relationship between the angle of internal friction of soil with numbers SPT

| SPT Penetration, N- | | |
|---------------------|-----------------|-------------------|
| Value (blows/ foot) | Density of Sand | (degrees) |
| <4 | Very loose | <30 |
| 4 - 10 | Loose | 30 - 35 |
| 10 - 30 | Medium | 35 - 40 |
| 30 - 50 | Dense | 40 - 45 |
| >50 | Very dense | >45 |

Value of the SPT in granular soils, is dependent on the Overhead pressure (\overline{v}_V) . So under the Effective pressure, the value of SPT (N) needed to corrected by:

 $N_{cor} = C_N N$

Several researchers such as (Peck et al., 1976), (Seed et al., 1976-1979) and (Tokimatsu and Yoshimi, 1983), Empirical relations for C_N have been proposed but The easiest with good accuracy by (Liao and Whitman, 1986) Proposed.

$$C_N = 9.78 \sqrt{\frac{1}{\sigma_V'(\text{KN}/m^2)}}$$

So:

 $\sigma_V = \gamma$

The two of input parameters (N_{corr} , L/B) For each soil sample are presented in the table 3. As you can see, For each model, Ratio of length to width of the foundation has changed until Dimension influence Settlement of Shallow Foundations to be on determined.

| sc | 24 | SN | И | SP | 1 | S | с | so | |
|-------|---------------|-------|---------------|--------|---------------|--------|---------------|-----------|---------------|
| N cor | $\frac{L}{B}$ | Ncor | $\frac{L}{B}$ | Ncor | $\frac{L}{B}$ | Ncor | $\frac{L}{B}$ | N_{cor} | $\frac{L}{B}$ |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| 8.5 | 4 | 9.48 | 6 | 15.5 | 8 | 7.74 | 8 | 7.74 | 3 |
| Tab | le 3: | Ratio | ofle | ngth t | o wi | dth ai | nd nu | mber | SPT |

| ab | le | 3: | Ratio | of | length | to | width | and | numb | er | SP | Τ |
|----|----|----|-------|----|--------|----|-------|-----|------|----|----|---|
|----|----|----|-------|----|--------|----|-------|-----|------|----|----|---|

| so | 4 | SN | Л | SN | 13 | SM | /13 | S | C4 |
|------|---------------|------|---------------|-----------------|---------------|----|---------------|------|---------------|
| N. | $\frac{L}{B}$ | N | $\frac{L}{B}$ | N _{er} | $\frac{L}{B}$ | N | $\frac{L}{B}$ | Nar | $\frac{L}{B}$ |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |
| 15.5 | 8 | 7.74 | 6 | 11 | 8 | 11 | 3 | 15.5 | 8 |

| S | 2 | SC | 2 | SC | 3 | S | C3 | S | C4 |
|---------------|---------------|------|---------------|------------------|---------------|------------------|---------------|------|---------------|
| $N_{\rm cor}$ | $\frac{L}{B}$ | Ncor | $\frac{L}{B}$ | N _{cor} | $\frac{L}{B}$ | N _{cor} | $\frac{L}{B}$ | Ncor | $\frac{L}{B}$ |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |
| 8.5 | 3 | 8.5 | 8 | 11.6 | 3 | 11.6 | 8 | 15.5 | 3 |

 Table 3. Ratio of length to width and number SPT

| SI | M3 | SI | VI 3 | s | C4 | SP | 1(3) | SC: | 2(3) |
|---------------|------|---------------|-------------|---------------|------|----|------|---------------|------|
| $\frac{L}{B}$ | N ar | $\frac{L}{B}$ | N_{\circ} | $\frac{L}{B}$ | Nar | | | $\frac{L}{B}$ | N ar |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |
| 3 | 11 | 8 | 11 | 3 | 15.5 | 3 | 15.5 | 3 | 8.5 |

Table 3. Ratio of length to width and number SPT

| C | н | Sc | 4 | SN | 1 | s | с | so | 3 |
|-----------------|---------------|----------------|---------------|-----------------|---------------|------|---------------|----|---------------|
| N _{or} | $\frac{L}{B}$ | N _w | $\frac{L}{B}$ | N _{ar} | $\frac{L}{B}$ | N | $\frac{L}{B}$ | N | $\frac{L}{B}$ |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |
| 7 | 6 | 15.5 | 6 | 9.48 | 6 | 7.74 | 6 | 6 | 11.6 |

Table 3. Ratio of length to width and number SPT

| 5 | Sm2 | 9 | Sm3 | 5 | Sp 1 | 5 | Sp 2 |
|---------------|------------------------------|---------------|------------------------------|---------------|------------------------------|---------------|------------------------------|
| $\frac{L}{B}$ | $N_{\scriptscriptstyle cor}$ |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |
| 6 | 11 | 6 | 14.4 | 6 | 15.5 | 6 | 18.2 |

| Table 3 | Ratio of | length t | to width | and | number | SPT |
|---------|----------|----------|----------|-----|--------|-----|
|---------|----------|----------|----------|-----|--------|-----|

2-4- Results of Analysis Plaxis Program

One of the Initial inputs of the neural network is the load on shallow foundations, Therefore, for each soil sample, We have considered 14 different loads to be sufficiently wide range of input data. After modeling the each samples under 14 different loads, the Settlement of Shallow Foundations is called output of Neural network.

| Sc2 (| 8) | SC3(| 3) | SC3(| 8) | SC4(: | 38) | SC4 (| 8) | SM(| 6) |
|--------|-----|--------|-----|--------|-----|--------|-----|--------|-----|--------|-----|
| δ | q | δ | q | δ | q | δ | q | δ | q | δ | q |
| 10.31 | 15 | 53.29 | 31 | 25.25 | 17 | 100.57 | 80 | 21.99 | 20 | 29.27 | 20 |
| 22.04 | 40 | 68.56 | 46 | 32.95 | 26 | 107.66 | 86 | 24.01 | 23 | 46.89 | 39 |
| 31.43 | 60 | 81 | 58 | 54.44 | 48 | 114.95 | 93 | 38.59 | 44 | 59.3 | 52 |
| 40.83 | 80 | 93.13 | 69 | 66.18 | 63 | 123.59 | 101 | 39.29 | 45 | 71.88 | 65 |
| 50.27 | 100 | 105.79 | 81 | 79.25 | 77 | 134.75 | 113 | 42.78 | 50 | 90.07 | 83 |
| 59.73 | 120 | 120.9 | 95 | 83.05 | 81 | 141.31 | 120 | 53.41 | 65 | 99.6 | 92 |
| 62.1 | 125 | 136.72 | 110 | 104.14 | 103 | 153.56 | 132 | 66.21 | 83 | 123.07 | 110 |
| 64.47 | 130 | 157.87 | 130 | 111.81 | 111 | 162.41 | 141 | 86.38 | 110 | 133.43 | 118 |
| 69.24 | 140 | 184.55 | 155 | 142.9 | 140 | 173.69 | 152 | 107.89 | 135 | 139.73 | 123 |
| 74.02 | 150 | 198.4 | 168 | 159.69 | 153 | 185.53 | 161 | 130.77 | 160 | 154.76 | 135 |
| 83.88 | 170 | 203.77 | 173 | 167.13 | 162 | 203.97 | 183 | 146.39 | 180 | 162.24 | 141 |
| 101.34 | 200 | 211.31 | 180 | 197.22 | 190 | 213.86 | 192 | 159.69 | 195 | 190.31 | 182 |
| 107.26 | 210 | 229.59 | 197 | 220.22 | 201 | 231.8 | 210 | 171.78 | 210 | 232.27 | 201 |
| 113.27 | 220 | 243.81 | 210 | 255.4 | 240 | 257.98 | 235 | 185.09 | 225 | 256.06 | 215 |

Table 4. Data obtained from the analysis of plaxis

| Sc 4 | (4) |) SM(6) | | (6) SP1(8) | | SC(8) | | SC (3) | | SC 2(3) | |
|--------|-----|---------|-----|------------|-----|--------|-----|--------|-----|---------|-----|
| δ | q | δ | q | δ | q | δ | q | δ | q | δ | q |
| 33.1 | 15 | 29.27 | 20 | 16.29 | 20 | 23.82 | 18 | 36.12 | 15 | 39.49 | 50 |
| 35.56 | 18 | 66.99 | 60 | 24.14 | 35 | 31.98 | 28 | 50.55 | 30 | 54.86 | 75 |
| 38.02 | 21 | 79.89 | 73 | 29.9 | 46 | 37.92 | 35 | 69.48 | 46 | 58.59 | 81 |
| 52.22 | 38 | 99.6 | 92 | 41.69 | 68 | 59.98 | 60 | 85.17 | 58 | 65.98 | 93 |
| 64.43 | 53 | 123.07 | 110 | 55.36 | 93 | 76.83 | 75 | 105.32 | 73 | 69.84 | 99 |
| 72 | 60 | 152.26 | 133 | 65.15 | 110 | 89.05 | 86 | 120.63 | 85 | 70.53 | 100 |
| 94.73 | 85 | 188.02 | 160 | 72.92 | 121 | 98.97 | 95 | 130.63 | 93 | 77.14 | 110 |
| 111.38 | 101 | 211.31 | 179 | 80.64 | 132 | 122.22 | 116 | 191.05 | 141 | 80.41 | 115 |
| 131.69 | 120 | 218.65 | 185 | 86.8 | 141 | 140.32 | 132 | 206.76 | 153 | 84.41 | 121 |
| 153.69 | 140 | 226 | 191 | 91.67 | 148 | 163.74 | 151 | 236.35 | 176 | 88.77 | 128 |
| 174.63 | 160 | 234.52 | 198 | 100.98 | 162 | 178.86 | 163 | 253.28 | 189 | 91.51 | 132 |
| 186.16 | 171 | 237.03 | 200 | 106.92 | 171 | 204.84 | 182 | 267.32 | 200 | 96.14 | 138 |
| 195.8 | 180 | 240.77 | 203 | 118.6 | 185 | 231.16 | 201 | 279.47 | 209 | 97.53 | 140 |
| 216.35 | 200 | 250.9 | 211 | 128.37 | 199 | 257.7 | 220 | 283.55 | 212 | 112.68 | 162 |

| | СН | | Sc 3 | | SM | | SC | | Sc 4 |
|-----|--------|-----|--------|-----|--------|-----|--------|-----|--------|
| q | δ | q | δ | q | δ | q | δ | q | δ |
| 5 | 13.6 | 10 | 18.42 | 3 | 15.31 | 1 | 4.16 | 15 | 17.6 |
| 6 | 14.68 | 20 | 26.1 | 7 | 19.11 | 5 | 6.5 | 21 | 21.27 |
| 25 | 36 | 30 | 34.31 | 20 | 31.8 | 38 | 26.39 | 29 | 26.54 |
| 45 | 58.6 | 38 | 40.78 | 38 | 49.94 | 66 | 47.03 | 55 | 43.27 |
| 55 | 69.99 | 44 | 45.75 | 56 | 68.65 | 93 | 71.08 | 69 | 53.06 |
| 70 | 87.17 | 61 | 59.99 | 80 | 93.92 | 121 | 98.87 | 73 | 55.76 |
| 74 | 91.78 | 70 | 68.89 | 98 | 113.39 | 132 | 110.78 | 81 | 61.7 |
| 89 | 109.23 | 89 | 93.26 | 119 | 136.41 | 150 | 130.46 | 108 | 89.71 |
| 100 | 122.16 | 100 | 106.69 | 160 | 187.01 | 180 | 162.73 | 120 | 100.41 |
| 110 | 134.28 | 115 | 123.36 | 190 | 225.63 | 200 | 186.29 | 133 | 111.51 |
| 130 | 162.63 | 120 | 128.57 | 215 | 258.58 | 208 | 195.65 | 160 | 133.49 |
| 180 | 239.69 | 145 | 154.36 | 218 | 262.53 | 222 | 212.87 | 200 | 165.49 |
| 200 | 272.62 | 160 | 168.96 | 225 | 272.1 | 250 | 248.12 | 200 | 179.09 |
| 240 | 341.96 | 183 | 193.3 | 243 | 296.29 | 255 | 254.8 | 220 | 181.84 |

Table 4. Data obtained from the analysis of plaxis

| Sc2 (| Sc2 (8) SC3(3) | | 3) | SC3(8) | | SC4(38) | | SC4 (8) | | SM(6) | |
|--------|----------------|--------|-----|--------|-----|---------|-----|---------|-----|--------|-----|
| δ | q | δ | q | δ | q | δ | q | δ | q | δ | q |
| 10.31 | 15 | 53.29 | 31 | 25.25 | 17 | 100.57 | 80 | 21.99 | 20 | 29.27 | 20 |
| 22.04 | 40 | 68.56 | 46 | 32.95 | 26 | 107.66 | 86 | 24.01 | 23 | 46.89 | 39 |
| 31.43 | 60 | 81 | 58 | 54.44 | 48 | 114.95 | 93 | 38.59 | 44 | 59.3 | 52 |
| 40.83 | 80 | 93.13 | 69 | 66.18 | 63 | 123.59 | 101 | 39.29 | 45 | 71.88 | 65 |
| 50.27 | 100 | 105.79 | 81 | 79.25 | 77 | 134.75 | 113 | 42.78 | 50 | 90.07 | 83 |
| 59.73 | 120 | 120.9 | 95 | 83.05 | 81 | 141.31 | 120 | 53.41 | 65 | 99.6 | 92 |
| 62.1 | 125 | 136.72 | 110 | 104.14 | 103 | 153.56 | 132 | 66.21 | 83 | 123.07 | 110 |
| 64.47 | 130 | 157.87 | 130 | 111.81 | 111 | 162.41 | 141 | 86.38 | 110 | 133.43 | 118 |
| 69.24 | 140 | 184.55 | 155 | 142.9 | 140 | 173.69 | 152 | 107.89 | 135 | 139.73 | 123 |
| 74.02 | 150 | 198.4 | 168 | 159.69 | 153 | 185.53 | 161 | 130.77 | 160 | 154.76 | 135 |
| 83.88 | 170 | 203.77 | 173 | 167.13 | 162 | 203.97 | 183 | 146.39 | 180 | 162.24 | 141 |
| 101.34 | 200 | 211.31 | 180 | 197.22 | 190 | 213.86 | 192 | 159.69 | 195 | 190.31 | 182 |
| 107.26 | 210 | 229.59 | 197 | 220.22 | 201 | 231.8 | 210 | 171.78 | 210 | 232.27 | 201 |
| 113.27 | 220 | 243.81 | 210 | 255.4 | 240 | 257.98 | 235 | 185.09 | 225 | 256.06 | 215 |

| Sc 4 | (4) | SM(| 6) | SP1(| 8) | SC(8 | 3) | SC (3) | | SC 2 | (3) |
|--------|-----|--------------------|-----|--------|-----|--------|-----|--------|-----|--------|------------------|
| δ | q | δ | q | δ | q | δ | q | δ | q | δ | q |
| 33.1 | 15 | 29.27 | 20 | 16.29 | 20 | 23.82 | 18 | 36.12 | 15 | 39.49 | 50 |
| 35.56 | 18 | 66.99 | 60 | 24.14 | 35 | 31.98 | 28 | 50.55 | 30 | 54.86 | 75 |
| 38.02 | 21 | 79.89 | 73 | 29.9 | 46 | 37.92 | 35 | 69.48 | 46 | 58.59 | 81 |
| 52.22 | 38 | <mark>99.</mark> 6 | 92 | 41.69 | 68 | 59.98 | 60 | 85.17 | 58 | 65.98 | 93 |
| 64.43 | 53 | 123.07 | 110 | 55.36 | 93 | 76.83 | 75 | 105.32 | 73 | 69.84 | 99 |
| 72 | 60 | 152.26 | 133 | 65.15 | 110 | 89.05 | 86 | 120.63 | 85 | 70.53 | 100 |
| 94.73 | 85 | 188.02 | 160 | 72.92 | 121 | 98.97 | 95 | 130.63 | 93 | 77.14 | 110 |
| 111.38 | 101 | 211.31 | 179 | 80.64 | 132 | 122.22 | 116 | 191.05 | 141 | 80.41 | 115 |
| 131.69 | 120 | 218.65 | 185 | 86.8 | 141 | 140.32 | 132 | 206.76 | 153 | 84.41 | 121 |
| 153.69 | 140 | 226 | 191 | 91.67 | 148 | 163.74 | 151 | 236.35 | 176 | 88.77 | 128 |
| 174.63 | 160 | 234.52 | 198 | 100.98 | 162 | 178.86 | 163 | 253.28 | 189 | 91.51 | 132 |
| 186.16 | 171 | 237.03 | 200 | 106.92 | 171 | 204.84 | 182 | 267.32 | 200 | 96.14 | 138 |
| 195.8 | 180 | 240.77 | 203 | 118.6 | 185 | 231.16 | 201 | 279.47 | 209 | 97.53 | 140 |
| 216.35 | 200 | 250.9 | 211 | 128.37 | 199 | 257.7 | 220 | 283.55 | 212 | 112.68 | <mark>162</mark> |

Table 4. Data obtained from the analysis of plaxis

| Smž | 2 | Sm: | 3 | Sp 1 | L | Sp | 2 |
|--------|-----|--------|-----|--------|-----|-------|-----|
| δ | q | δ | q | δ | q | δ | q |
| 13.55 | 3 | 27.46 | 30 | 15.52 | 20 | 4.01 | 3 |
| 17.63 | 8 | 41.15 | 50 | 28.29 | 46 | 5.29 | 8 |
| 25.03 | 17 | 52.15 | 66 | 67.33 | 108 | 10.53 | 26 |
| 40.77 | 35 | 65.16 | 85 | 84.72 | 133 | 14.39 | 39 |
| 68.91 | 66 | 80.86 | 107 | 108.09 | 169 | 34.76 | 101 |
| 81.92 | 79 | 86.57 | 115 | 115.78 | 181 | 41.49 | 120 |
| 100.04 | 100 | 104.65 | 140 | 127.87 | 199 | 48.74 | 140 |
| 134.2 | 120 | 128.87 | 173 | 128.57 | 200 | 54.15 | 155 |
| 162.56 | 143 | 146.42 | 191 | 136.07 | 211 | 60.54 | 173 |
| 187.43 | 165 | 153.79 | 200 | 142.04 | 220 | 67.31 | 191 |
| 206.36 | 181 | 176.04 | 231 | 150.01 | 231 | 74.39 | 210 |
| 229.1 | 200 | 183.58 | 240 | 155.03 | 238 | 79.14 | 223 |
| 253.51 | 220 | 185.27 | 242 | 157.01 | 241 | 82.08 | 231 |
| 259.6 | 225 | 187.81 | 245 | 159.83 | 245 | 84.47 | 238 |

Table 4. Data obtained from the analysis of plaxis

| 0000.5 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 0000.5 | 8.0000 | 8.0000 |
|-----------|------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 |
| Columns 3 | 20 through | 330 | | | | | | | | |
| | | | | | | | | | | |
| | 161.0000 | | | 45.0000 | | 70.0000 | | | 110.0000 | |
| 6.0000 | 6.0000 | 6.0000 | | | 8.0000 | | 8.0000 | 8.0000 | 8.0000 | 8.0000 |
| 11.0000 | 11.0000 | 11.0000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 |
| olumns 3 | 31 through | 341 | | | | | | | | |
| 52.0000 | 178.0000 | 192.0000 | 211.0000 | 220.0000 | 230.0000 | 15.0000 | 30.0000 | 46.0000 | 58.0000 | 73.0000 |
| 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 |
| 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 |
| olumns 3 | 42 through | 352 | | | | | | | | |
| 81.0000 | 96.0000 | 102.0000 | 115.0000 | 121.0000 | 132.0000 | 145.0000 | 162.0000 | 182.0000 | 15.0000 | 32.0000 |
| 3.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 | 8.0000 | 8.0000 |
| 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 15.5000 | 11.0000 | 11.0000 |
| olumns 3 | 53 through | 363 | | | | | | | | |
| 52.0000 | 64.0000 | 73.0000 | 82.0000 | 93.0000 | 110.0000 | 135.0000 | 142.0000 | 156.0000 | 167.0000 | 182.0000 |
| 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 | 8.0000 |
| 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 |
| olumns 3 | 64 through | 374 | | | | | | | | |
| 00.0000 | 45.0000 | 56.0000 | 73.0000 | 85.0000 | 92.0000 | 101.0000 | 115.0000 | 120.0000 | 132.0000 | 146.0000 |
| 8.0000 | 3,0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 | 3.0000 |
| 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11.0000 | 11,0000 |
| olumns 3 | 75 through | 378 | | | | | | | | |
| 155.0000 | 168.0000 | 181.0000 | 195.0000 | | | | | | | |
| 3.0000 | 3.0000 | 3.0000 | 3.0000 | | | | | | | |
| | | | | | | | | | | |

Figure 6. P matrix

2-5- Input data into the MATLAB program

Input data are entered in MATLAB as a matrix. we define 3 initial input to the neural network and We had 27 models, each of which had 14 different types of loading, Thus, for each input, there will be 378 data. **2-5-1- P matrix**

This matrix is called as the neural network input matrix and contains: q, N (N_{cor}), Z (L/B) and In Matlab is defined as p=[q;z;n] so that shown in Figure 6

2-5-2-Output matrix of the neural network (t):

This Matrix with dimensions (1×378) is the output of the neural network as the Settlement of Shallow Foundations obtained by analyzing samples is modeled by the plaxis program called t matrix that shown in Figure 7.

2-5-3-Defines the structure of an artificial neural network

In this project, the multi-layer perceptron network as the most used type of artificial neural network in solving engineering problems was used. Figure 5.

2-6-Network code in MATLAB is given below



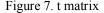
Neural network training function is **trainlm**. After the data for classification and regression functions affected by this function, the learning process is to achieve a good correlation. in Figure 8 is an overview of the network.

Perceptron neural network with two layers and a middle layer that is hidden in the hidden layer There are 350 hidden neuron is composed of a single output of the network is taken. Code is as follows:

net=newff ([1 255;3 6;7 18.2], [350 1], {'tansig' 'purelin'},'trainlm)

ANN training code: Net 1 = train (net, P,T)

t=[13.6 14.68 36 58.6 69.99 87.17 91.78 109.23 122.16 134.28 162.63 239.69 272.62 341.96 15.31 19.11 31.8 49.94 68.65 93.92 113.39 136.41 187.01 225.63 258.58 262.53 272.10 296.29 4.16 6.5 26.39 47.03 71.08 98.87 110.78 130.46 162.73 186.29 195.65 212.87 248.12 254.8 18.42 26.1 34.31 40.78 45.75 59.99 68.89 93.26 106.69 123.36 128.57 154.36 168.96 193.3 17.6 21.27 26.54 43.27 53.06 55.76 61.7 89.71 100.41 111.51 133.49 165.49 179.09 181.84 13.55 17.63 25.03 40.77 68.91 81.92 100.04 134.2 162.56 187.43 206.36 229.1 253.51 259.6 27.46 41.15 52.15 65.16 80.86 86.57 104.65 128.87 146.42 153.79 176.04 183.58 185.27 187.81 15.52 28.29 67.33 84.72 108.09 115.78 127.87 128.57 136.07 142.4 150.01 155.03 157.01 159.83 4.01 5.29 10.53 14.39 34.76 41.49 48.74 54.15 60.54 67.31 74.39 79.14 82.08 84.47 33.1 35.56 38.02 52.22 64.43 72 94.73 111.38 131.69 153.15 174.63 186.16 195.8 216.35 29.27 66.99 79.89 99.6 123.07 152.26 188.02 211.31 218.65 226 234.52 237.03 240.77 250.9 16.29 24.14 29.9 41.69 55.36 65.15 72.92 80.64 86.8 91.67 100.98 106.92 118.6 128.37 23.82 31.98 37.92 59.98 76.83 89.05 98.97 122.22 140.32 163.74 178.86 204.84 231.16 257.7 36.12 50.55 69.48 85.17 105.32 120.7 130.63 191.05 206.76 236.35 253.28 267.32 279.47 283.55 39.49 54.86 58.59 65.98 69.84 70.53 77.14 80.44 84.41 88.77 91.51 96.14 97.53 112.68 10.31 22.04 31.43 40.83 50.27 59.73 62.1 64.47 69.24 74.02 83.88 101.34 107.26 113.27 53.29 68.56 81 93.13 105.79 120.9 136.72 157.87 184.55 198.4 203.77 211.31 229.59 243.81 25.25 32.95 54.44 66.18 79.25 83.05 104.14 111.81 142.9 159.69 167.13 197.22 220.22 255.4 100.57 107.66 114.95 123.59 134.75 141.31 153.56 162.41 173.69 185.53 203.97 213.86 231.8 257.98 21.99 24.01 38.59 39.29 42.78 53.41 66.21 86.38 107.89 130.77 146.39 159.69 171.78 185.09 29.27 46.89 59.3 71.88 90.07 99.6 123.07 133.45 139.73 154.76 162.24 190.31 233.27 256.06 24.93 29.53 43.79 56.39 64.21 76.12 89.2 101.28 118.69 130.71 139.74 163.33 206.14 218.88 35.33 44.41 57.88 72.88 86.55 93 119.37 135.34 155.48 164.44 174.22 191.12 232.12 247.18 28.89 39.29 46.27 56.98 68.35 78.82 86.38 107.89 123.82 143.27 157.52 172.75 180.96 189.74 32.07 43.94 57.12 63.11 92.57 102.2 118 15 124 29 136 6 142 28 153 56 167 66 184 52 202 95 24 93 40 98 60 33 72 12 81 05 90 01 101.28 118.69 149.39 158.26 176.21 188.44 208.7 232.03 71.91 84.14 105.81 123.11 133.93 147.05 167.39 174.72 191.69 211.13 223.81 241.74 259.43 278.45



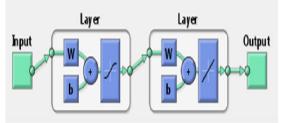


Figure 8. Overview of network

The network codes is the error rate of the network can be set so that the desired error rate reached a certain stage.

net.trainParam.show = 50; net.trainParam.lr = 0.05; net.trainParam.epochs =1000; net.trainParam.goal = 1e-3 3- Results and discussion

With all of the steps described, the Neural network error rate has reached **0.98125**. This figure 9, shows a good training program to suit a wide range of input data networks.

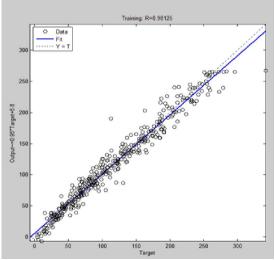


Figure 9 –a. Neural network performance

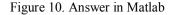
The code can be used to query the network. a= sim (net1, P);

For example, soils The ratio of length to width 6 and number oo SPT 14.4, Plaxis Program, the answer is **128.87** and A neural network designed **129.0209** gives an approximate answer is acceptable.

Below this number is shown in the MATLAB programming environment. The question of the program is as follows:

a= sim (net1, [173;6;17.4])

```
>> net1 = train(net, p, t);
>> a= sim(net1,[173;6;14.4]);
>> a= sim(net1,[173;6;14.4])
a =
129.0209
```



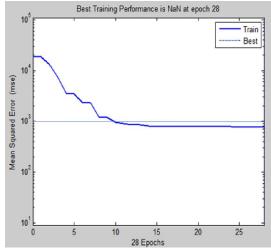


Figure 9-b. Best Training Performance of the Network

3-1- Influence Of neurons in the hidden layer on R

Given the importance of this issue in regression neural network input data so The number 350 was used in the artificial neural network which is the value obtained experimentally.

If: net=newff ([1 255;3 8;7 18.2], [320 1], {'tansig' 'purelin'},'trainlm');

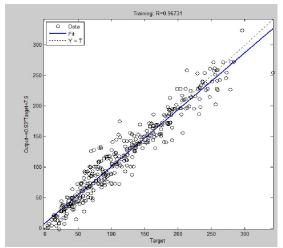


Figure 11-a. Amount of R in 320 Neron is 0.96731

If: net=newff ([1 255;3 8;7 18.2], [360 1], {'tansig' 'purelin'},'trainlm');

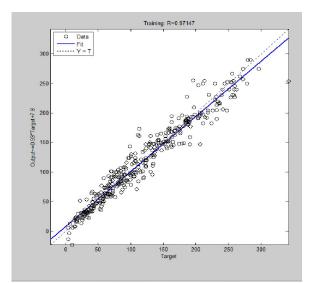


Figure 11-b. Amount of R in 320 Neron is 0.9714

4. Conclusion

The data from the neural network being used as a test of the soil was SC3 with The ratio of length to width is 8. The results of the Settlement by using neural network has a good agreement with the results of Plaxis and All results are shown in Table 5.

4-2-Dimensions Foundation effects on Settlement

Soil samples were taken to be SC4. The parameters are shown in Table. The soil under the 4 Different Dimensions foundation and the load $100 \frac{Kg}{m^2}$. The coordinates of the selected point by (11,12.5) to calculate the rate of change of meeting dates and results of these studies are shown in Figure 12.

Curve A: Of the soil friction angle SC4 is 39 degrees under a uniform load of $100 \frac{\text{Kg}}{m^2}$ On shallow foundations with length to width ratio is 3. (6 meters long and 2 meters wide).

Curve B: Of the soil friction angle SC4 is 39 degrees under a uniform load of $100 \frac{\text{Kg}}{\text{m}^2}$ On shallow foundations with length to width ratio is 4. (8 meters long and 2 meters wide).

| SC | ANN Results | | | |
|-----------------------|----------------------|--------------------------|--|--|
| q($\frac{KN}{m^2}$) | $\delta (10^{-3}mm)$ | δ (10 ⁻³ mm) | | |
| 52 | 60.33 | 55.53 | | |
| 59 | 67.23 | 63.93 | | |
| 60 | 68.21 | 63.75 | | |
| 65 | 73.11 | 66.86 | | |
| 75 | 83.12 | 85.03 | | |
| 80 | 88.19 | 78.76 | | |
| 100 | 108.41 | 107.145 | | |
| 111 | 119.72 | 115.37 | | |
| 117 | 125.91 | 117.43 | | |
| 120 | 129.42 | 123.94 | | |
| 135 | 149.39 | 140.93 | | |
| 140 | 155.46 | 147.59 | | |
| 150 | 168.28 | 157.2 | | |
| 160 | 180.22 | 172.03 | | |

Table 5. A comparison of neural network and applications

Curve C: Of the soil friction angle SC4 is 39 degrees under a uniform load of $100 \frac{\kappa_g}{m^2}$ On shallow foundations with length to width ratio is 8. (8 meters long and 1 meters wide).



Figure 12. Dimensions Foundation effects on Settlement

Curve A: Of the soil friction angle SC4 is 39 degrees under a uniform load of $100 \frac{\text{Kg}}{m^2}$ On shallow foundations with length to width ratio is 3. (6 meters long and 2 meters wide).

Curve B: Of the soil friction angle SC4 is 39 degrees under a uniform load of $100 \frac{\text{Kg}}{m^2}$ On shallow foundations with length to width ratio is 4. (8 meters long and 2 meters wide).

Curve C: Of the soil friction angle SC4 is 39 degrees under a uniform load of $100 \frac{\text{Kg}}{m^2}$ On shallow foundations with length to width ratio is 8. (8 meters long and 1 meters wide).

Curve D: Of the soil friction angle SC4 is 39 degrees under a uniform load of $100 \frac{\text{Kg}}{m^2}$ On shallow foundations with length to width ratio is 6. (6 meters long and 1 meters wide).

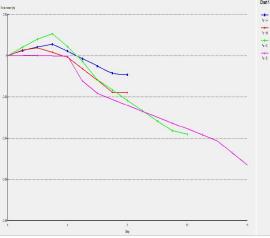


Figure 13. Angle of internal friction curve effects

4-3- Angle of internal friction effects

To evaluate the influence of internal friction angle of a soil sample in a Amount of Settlement s, at one point considered for the analysis of soil SC4.

A type of foundation and the load, the changes we observed the effects of friction.

Curve A: Of the soil friction angle SC4 is 39 degrees under a uniform load of $100 \frac{\text{Kg}}{\text{m}^2}$ On shallow foundations with length to width ratio is 4. (8 meters long and 2 meters wide).

Curve B: Of the soil friction angle SC4 is 45 degrees under a uniform load of $100 \frac{\text{Kg}}{\text{m}^2}$ On shallow foundations with length to width ratio is 4. (8 meters long and 2 meters wide).

Curve C: Of the soil friction angle SC4 is 30 degrees under a uniform load of $100 \frac{\text{Kg}}{\text{m}^2}$ On shallow foundations with length to width ratio is 4. (8 meters long and 2 meters wide).

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Curve D: Of the soil friction angle SC4 is 35 degrees under a uniform load of $100 \frac{Kg}{m^2}$ On shallow foundations with length to width ratio is 4. (8 meters long and 2 meters wide).

As is known in the form of increasing the amount of soil friction angle, the highest Settlement in the lower reaches Also, the curves A and B Against two curves are much more friction, the Settlement is also lower than the other two curves.

Increase the contact area of foundation soil was modeled on, the settlement amount will be reduced. Distribution of the stress distribution in the soil layers below the foundation would be better and reduce the stress level in the soil layers and also to reduce the amount of foundation settlement.

Increase the friction angle of the soil in a layer of soil to reduce settlement will increase the contact area between the particles of the soil layer will be.

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