**To Examination on Optimum Utilisation of Kinetic Energy and Operational Features from Tidal Stream Turbine**

Madan D1, Dr Rajendran M2

1. Research Scholar, Department of Mechanical Engineering, Anna University Chennai, Tamilnadu, India
2. Professor and Head, Department of Mechanical Engineering, Government College of Technology, Coimbatore, Tamilnadu, India.

Email: [madan.research@gmail.com](mailto:madan.research@gmail.com)

**Abstract:** Tidal stream energy represents a large resource along the power inflow of a current follows a cubic law and the tidal stream energy is only attractive where the current exceeds 2m/s during a sufficient time along the year. Some examples of the theoretical resource are shown for different sites and tide amplitude. The tidal stream velocity varies along the day and the month. The theoretical output is discussed for a typical site in terms of instantaneous power and annual production. For a given site and rotor diameter, economical factors invite to limit the electrical capacity to an economical optimum. The main features of the Marenergie type of tidal stream turbine are presented. The design has been governed by the following considerations: (a) This source of renewable energy must have an acceptable cost, so the overall concept must be economically viable (b) The tidal turbine must work in a submarine environment where maintenance is very difficult and the machinery must be made as simple as possible (c) All marine operations for installation and maintenance must take into account the strong currents prevailing in the potential sites (d) A compromise must be found between the capital cost and the yearly energy production and (e) The interaction of the waves with the current must be considered.

**[**Madan D, Rajendran M. **To Examination on Optimum Utilisation of Kinetic Energy and Operational Features from Tidal Stream Turbine.** *Cancer Biology* 2016;6(4):180-184]. ISSN: 2150-1041 (print); ISSN: 2150-105X (online). <http://www.cancerbio.net>. 10. doi:[10.7537/marscbj060416.10](http://www.dx.doi.org/10.7537/marscbj060416.10).

**Keywords**: Tidal, turbines, stream, current, rotor and wave

**1. Introduction**

The kinetic energy of the currents can be harnessed by submarine tidal turbines. The physical phenomena involved must be investigated before designing the suitable equipment. The actual resource on a given site can be predicted if the local tidal streams are known, but the influence of the wave climate must also be considered.

**The tidal stream resource**



Figure 1: Typical current variation with time during a mean spring tide

As a first approach, the power of the water stream through a tidal turbine rotor follows a cubic law similar to the power law of a wind turbine. This equation shows that tidal stream energy is attractive where the tide creates strong currents. The suitable zones are found where the coast configuration restricts the tide propagation, around capes, between islands, in limited water depth areas. The water depth is limited to less than 50m. The overall theoretical resource is estimated at several gigawatts.



Figure 2: Variation of the tide coefficient

The tidal stream velocity varies along the day and the month. Figure 2 shows the value of the tide coefficient for Brest along the year 2001. The mean spring tide has a coefficient of 95, while the mean neap tide coefficient is 45. The power output is then variable along the time and varies from day to day. Figure 3 shows the theoretical power input taking into account the equation [1]. The power inflow is notably stronger during spring tides than during neap tides.



Figure 3: Power inflow variation during a mean spring tide and a mean neap tide

The current velocity can be predicted at any moment of the year. It is then possible to calculate how many hours per year a given power inflow is observed, as illustrated on figure 4.



Figure 4: Cumulative distribution of the power inflow on a site with a maximum velocity of 3 m.s-1 during mean spring tide

The electrical generator of the turbine is characterized by its nominal power. The power input a rotor is able to exploit is then limited by the generator rating. When the current brings more power than this rating, the power is restricted to the nominal power and the excess of energy is lost. The theoretical resource is then a function of the turbine rating, as shown on figure 5. If high nominal power ratings are selected, the benefit on the energy production is marginal. Figures 4 and 5 represent the power inflow of the current. The actual electrical power must take into account the power coefficient of the turbine. Dividing the annual energy by the nominal power yields the equivalent number of hours of production. Figure 6 presents the values obtained, together with the number of hours at full load for the same example. The investment cost of the turbine is a function of the power rating of the generator. Therefore, there is an optimum economical design which is considered to correspond to an equivalent production time of 2500 hours to 3000 hours per year. The optimum rating depends on the site conditions.



Figure 5: Relationship between the power input rating and the annual theoretical energy resource



Figure 6: Relationship between the nominal power rating and the hours of production per year

**2. Material and Methods**

**2.1 The Marenergie tidal turbine**

When designing a tidal turbine, the following parameters must be taken into consideration: (a) The turbine must work in a submarine environment where maintenance is very difficult, so the machinery must be made as simple as possible (b) All marine operations for installation and maintenance must take into account the strong currents prevailing in the areas of interest (c) A compromise must be found between the capital cost and the yearly energy production and (d) The interaction of the waves with the current must be considered. The above mentioned facts led to the following solutions for the design of the turbine: (a) The rotor is maintained fixed in the space and the water flows alternatively in both directions during flood and ebb flows and (b) The number of moving parts exposed to the sea water is kept to a minimum. The blades are fixed and welded onto the hub. The only moving part in sea water requiring some attention is the seal of the rotor shaft on the nacelle front face. The consequences of these choices are: (a) The rotor turns in both directions following the current direction and (b) The blades are symmetrical: Both ends are alternatively leading and trailing edges.

The peripheral velocity is kept at a relatively low level (7m.s-1) in order to avoid cavitations phenomena on the blades. The optimum velocity decreases when the number of blades is increased, and a correct velocity is obtained with 6 blades. The preliminary studies indicate the benefit of a circular belt at the rotor periphery. This enhances the blade efficiency and eliminates most of the potential vibrations. It should also limit the emission of low frequency noise at the blade tips. The actual design of the base depends on the soil nature. The rotor may be surrounded by a duct if required. Several turbines can be arranged in arrays as shown on figure 8. This increases the power collected locally and allows a better use of the submarine cable connecting the array to the grid onshore.

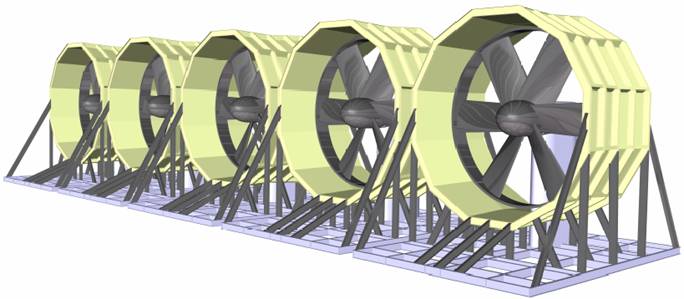


Figure 8: Schematic view of an array of Marenergie ducted turbines



Figure 9: Typical characteristics of a Marenergie tidal turbine

A computer model of a rotor with symmetrical blades has been made. Figure 9 presents the power output of the rotor, as a function of the current velocity and the rotation speed. For a given current there is an optimum rotation speed giving a power maximum. The figure also shows that the power is cancelled for a rotation speed called free wheeling speed, slightly higher than the optimum speed.

As discussed earlier, it is not advisable to use the maximum hydraulic power of the turbine when the current is particularly strong. The electrical generator is designed with a nominal power of 200 kW. When the current is sufficient, the power output is kept at this level. The rotor is then stabilized at a rotation speed corresponding to the equivalent hydraulic power. Figure 9 shows that this operation mode is stable. If for instance the rotor slows down for any reason, its hydraulic power increases and this causes the rotor to accelerate and return to the correct rotation speed.

The generator must be a variable speed type. It can be either an asynchronous machine with a wounded rotor fed by a separate variable frequency current or a synchronous machine with electromagnets or permanent magnets. Such generators are now extensively used in wind turbines.

**3. Results**

**3.1 Wave current interaction**

The water is put into movement not only by the tidal streams, but also by the wave action. The combination of both movements is a complex problem. In particular, it is known that a current flowing against the swell increases the wave height while the waves are attenuated when both phenomena are in the same direction. A discussion of the problem can be found in the literature and is subject to further research (2).

A regular swell traveling over an area of constant water depth is characterized by the height between crest and trough **H** and a period **T**. The distance between two successive crests is the wave length **L** which can be calculated by the following implicit relation:

 [2]

where is the acceleration of gravity (9.81 m.s-2) and **d** is the water depth in the absence of waves.

The amplitude of the wave movement decreases with the depth **z** below the surface. The horizontal velocity **Vx** induced by the wave action is given by the formula:

 [3]

In the absence of wave, the current velocity is zero on the seabed and highest at the surface. The velocity profile is generally approached by the following relationship between the elevation above the seabed and the local velocity:

 [4]



Figure 10: Influence of the swell (H= 2m - T = 9s) on the velocity profiles – Water depth = 30m

It is assumed that the velocity of the water particles is the sum of the values given by the equations [3] and [4]. Figure 10 presents an example with a swell traveling in the same direction as the current. The velocity fluctuates at the frequency of the swell between a minimum and a maximum value. There is also a vertical gradient which can induce a bending force on the rotor shaft. A duct around the rotor may equalize the velocity throughout the rotor plane and reduce this effect. The inertia of a tidal turbine is relatively low compared to the mass of water flowing through the rotor. When the water velocity fluctuates under the influence of the waves, the rotor spinning velocity follows very rapidly. An example is presented on the figure 11 when the current and the waves are aligned.



Figure 11: Behavior of the tidal turbine: Current = 3 m.s-1 - Swell: H= 2m T= 9s

It can be seen in this example that the power which would be constant and equal to the nominal value in the absence of waves decreases during a fraction of the wave period. In order to obtain a constant output from a single turbine, the generator should be operated at a power level corresponding to the lowest power value during the wave period. The figure 12 shows the power calculated accordingly in the case of a regular swell, for different wave heights and wave periods for a depth of 30m. The results could be different with a generator technology able to accept temporary power surges above the nominal power. A smoothing of the production would be obtained, with a higher average output.



Figure 12: Typical power output of a single turbine with waves aligned with the current

The actual effect of the waves on the energy production must be calculated for each site, taking into account the local wave climate. The effect of the velocity fluctuations on the tidal turbine is similar to the turbulence on wind turbines. The design of the machinery must take into consideration the fatigue resulting from these fluctuations. When several turbines are installed on the site, the swell does not interfere with all the rotors at the same moment provided the swell front is not aligned with the array of turbines. There is an averaging effect which levels out the fluctuations. Figure 13 shows that it is even possible to obtain more power in the case of a low current when waves are superposed.



Figure 13: Average output of an array of turbines ideally spaced along the wave length

**4. Conclusion**

Tidal turbines can be optimized according to the local conditions prevailing on the different sites. The Marenergie tidal turbine is designed as simple as possible. Variable speed generators are required, similar to the types used in modern wind turbines. Waves may create power fluctuations and fatigue which must be taken into account in the sizing of the equipment. When assessing the potential energy productivity of a site, the local wave climate must be considered in addition to the tidal currents. The layout of the turbine arrays can be arranged in order to minimize the detrimental effect of the waves. The horizontal axis rotor is fixed in space. It is made of welded symmetrical blades which can accept the current from both sides. For a given current velocity, there is a rotation speed delivering the maximum power and a freewheeling rotation speed. The design of the electrical equipment and the operation philosophy takes this behavior into account. Waves interfere with the current and this causes power fluctuations. The wave action can severely limit the acceptable output of a single turbine, but the result is different for an array of many turbines.

**Correspondence Author:**

Madan D

Research Scholar

Department of Mechanical Engineering

Anna University Chennai

Chennai, Tamilnadu, India

Email: madan.research@gmail.com

**References**

1. Divers aspects de l’exploitation de l’énergie des courants marins – Daviau – Majastre – Guéna Ruer – Seatechweek 2004 – Brest.
2. Dronkers, J.J., 1964. Tidal Computations in Rivers and Coastal Waters. North-Holland Publishing Company, Amsterdam, 518pp.
3. Fu, L.-L., 1981. Observations and models of inertial waves in the deep ocean. Reviews of Geophysics and Space Physics 19, 141–170.
4. Gerkema, T., 2001. Internal and interfacial tides: beam scattering and local generation of solitarywaves. Journal of Marine Research 59, 227–255.
5. Huthnance, J.M., Baines, P.G., 1982. Tidal currents in the northwest African upwelling region. Deep-Sea Research 29, 285–306.
6. Magaard, L., McKee, W.D., 1973. Semi-diurnal tidal currents at ‘site D’. Deep-Sea Research 20, 997–1009.
7. Wave curent interactions – Jonsson - The Sea – I-1990 pp. 65-120, Editors B. LeMehaute and D. Hanes, J. Wiley, New York.

12/25/2016